

Highway Geometric Design

Masoud Ghodrat Abadi, PhD
Rohollah (Roham) Moghadam, PhD



Learning Objectives

- 1 **Describe** the role of highway geometric design in providing safe and efficient roadways.
- 2 **Identify** the main components of roadway alignment: horizontal, vertical, and cross-sectional.
- 3 **Interpret** stationing notation to locate points along a roadway alignment.
- 4 **Recognize** key terminology and geometry of vertical curves, including PVC, PVI, and PVT.
- 5 **Explain** the concept of stopping sight distance and how it differs for crest and sag curves.
- 6 **Identify** common horizontal curve types and their basic geometric elements.

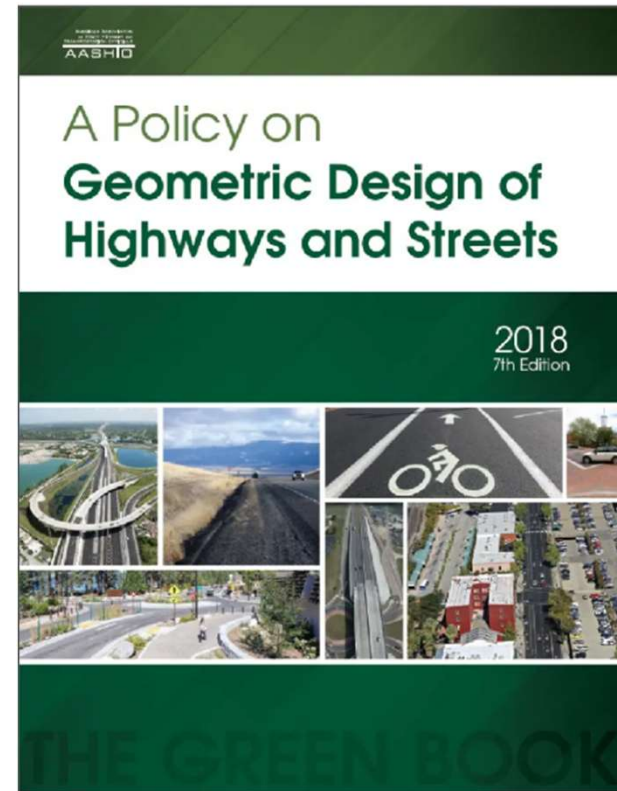
Introduction

- Geometric Design Philosophy:
 - **Safety and Efficiency**
 - Safe roadway features that provide adequate **Stopping Sight Distance** and/or **Passing Sight Distance**
- Geometric Design is based on the following factors:
 - The design **driver**
 - The design **vehicle**
 - The design **environment**



Introduction

- Current guidelines for highway design are presented in detail in **A Policy on Geometric Design of Highways and Streets**
 - Published by the American Association of State Highway and Transportation Officials (AASHTO)
 - Commonly known as “**The Green Book**”



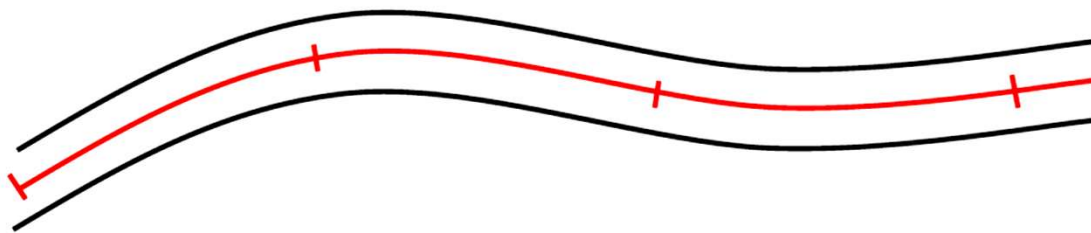
Principles of Roadway Alignment

- **Stationing**

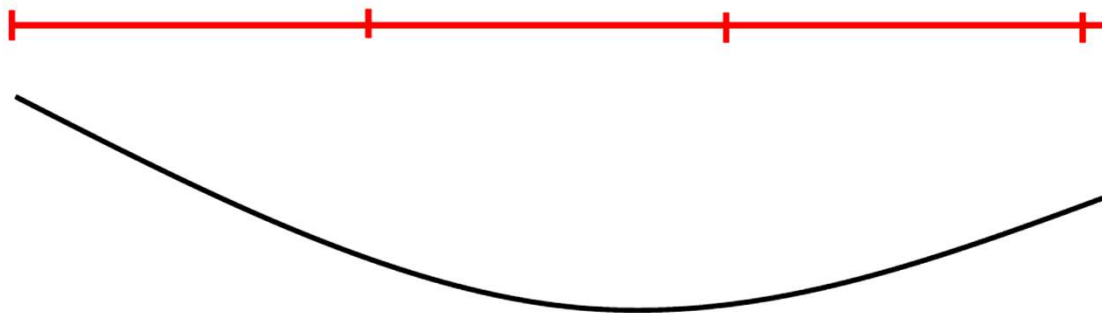
- To locate an alignment (Horizontal or Vertical)
- In **U.S. customary** units, each station consists of 100 ft. of horizontal distance:
 - Origin station denoted as 0 + 00.00
 - A point 685.3 ft. from the origin would be at station 6 + 85.30 (six stations and 85.3 ft.)
- In **metric** units, each station consists of 1000 m of horizontal distance:
 - Origin station denoted as 0 + 000.000
 - A point 2213.5 m from the origin would be at station 2 + 213.500 (two stations and 213.5 m)

Principles of Roadway Alignment

Horizontal Alignment



Vertical Alignment



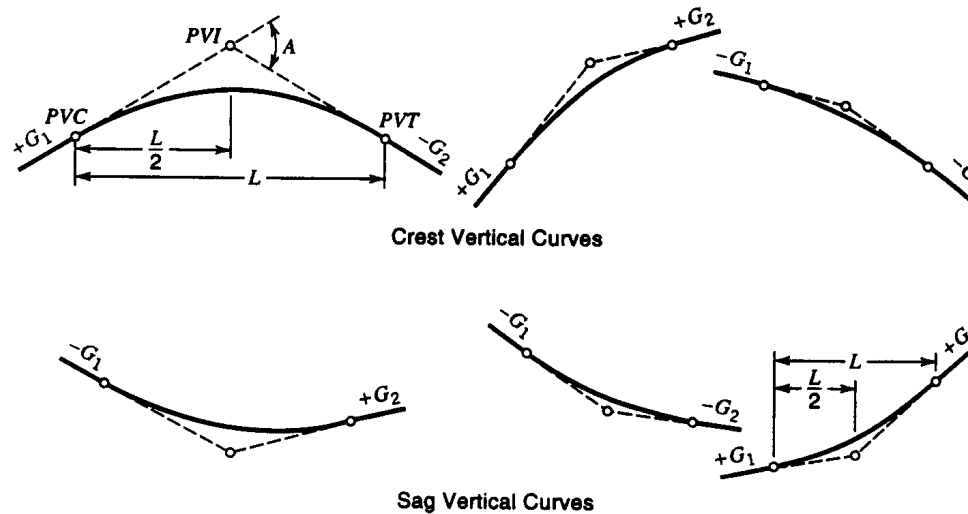


Vertical Alignment

Notation

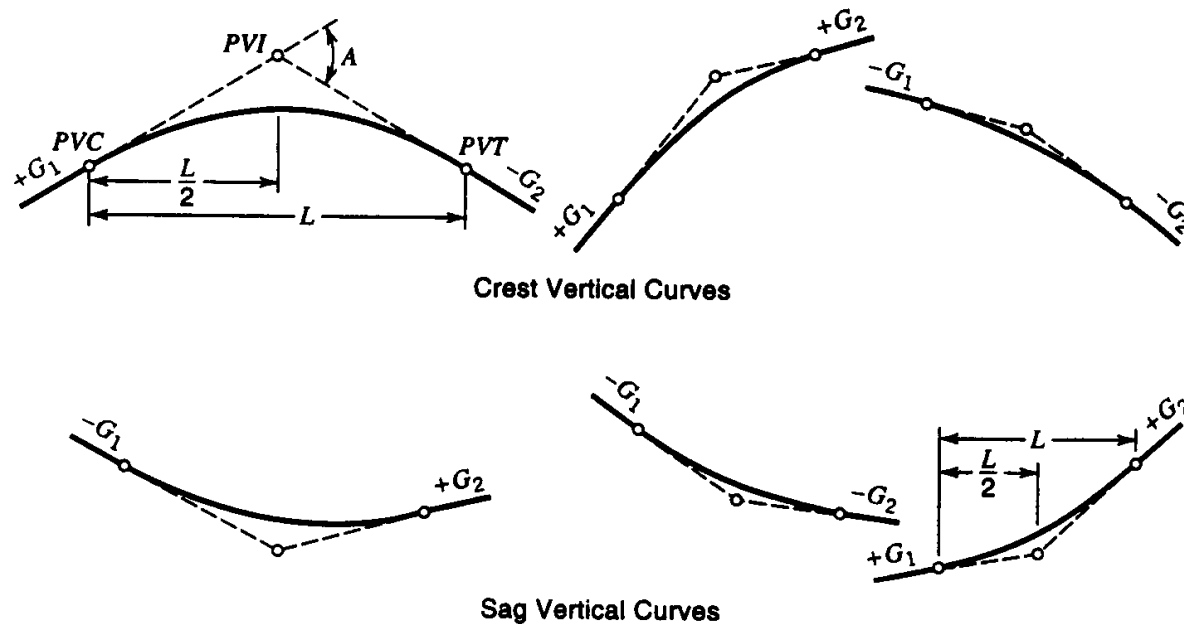
- Curve Points

- PVC: Point of Vertical Curvature (beginning of curve)
- PVI: Point of Vertical Intersection (intersection of tangents)
- PVT: Point of Vertical Tangent (ending point of curve)



Terminology

- Sag vs. Crest Vertical Curves



Vertical Curve Equations

- Elevations along a **Vertical Curve** is generally given by a **Parabolic Curve**.
 - Parabolic function $\rightarrow y = ax^2 + bx + c$
 - where y is the elevation of a point on the curve from the PVC and x is a horizontal distance from the PVC.

y = roadway elevation
x = distance from PVC
c = elevation of PVC

- Equal Tangent Vertical Curves
 - PVI is always L/2 from PVC

$$a = \frac{(G_2 - G_1)}{2L}$$
$$b = \frac{dy}{dx} = G_1$$
$$c = \text{PVC elevation}$$

Stopping Sight Distance (SSD)

- It is necessary, when designing vertical curves, to provide adequate **Stopping Sight Distance (SSD)**
- curve construction is expensive, we want to minimize curve length, subject to adequate SSD
- The **minimum stopping distance** is the distance required to bring a vehicle traveling at a give speed to a stop after an object on the road becomes visible.

Stopping Sight Distance (SSD)

- Stopping Sight Distance is a function of distance travelled during perception/reaction time and distance travelled to bring the vehicle to a stop.

$$SSD = \frac{V_1^2}{2g\left(\frac{a}{g} \pm G\right)} + V_1 t_r$$

where

SSD is the stopping sight distance in feet.

V_1 is the initial vehicle speed in ft/s.

g is gravitational constant, 32.2 ft/s².

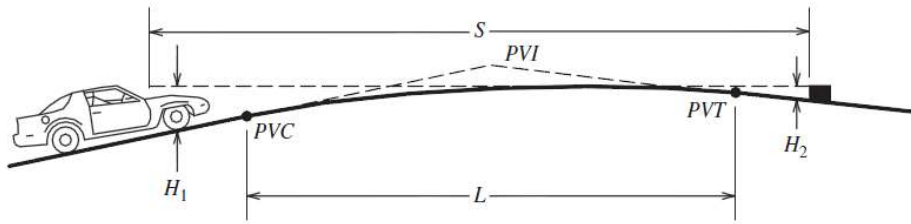
a is deceleration in ft/s². (**Assume 11.2 ft/s²**).

G is roadway grade (+ uphill, – downhill) in decimals (% / 100)

t_r is driver perception/reaction time in sec (**Assume 2.5 sec.**)
[1.0 sec if expected; 2.5 sec if unexpected]

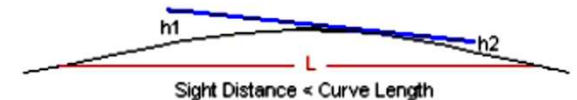
SSD on Crest Curves

- The curve length is critical to proving ample stopping distance to avoid hitting an object.



- **Sight distance (S)**
- Driver's eyes (H_1)
- Height of an object (H_2)
- Equal tangent curve (use parabola properties)

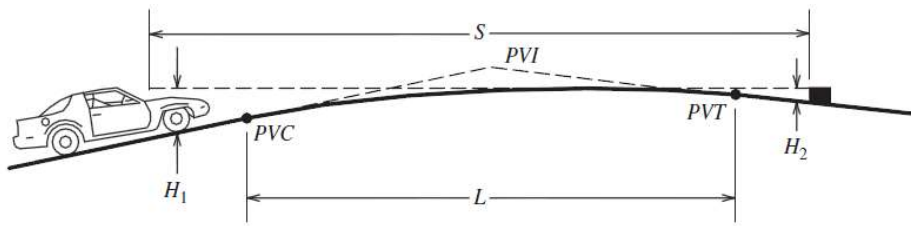
- If $S < L$ (you can't see the end of the curve):



$$L_m = \frac{A \times SSD^2}{200(\sqrt{H_1} + \sqrt{H_2})^2}$$

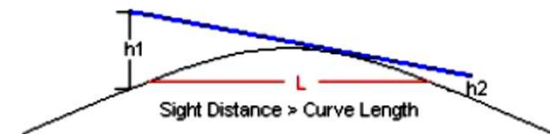
SSD on Crest Curves

- The curve length is critical to proving ample stopping distance to avoid hitting an object.



- **Sight distance (S)**
- Driver's eyes (H_1)
- Height of an object (H_2)
- Equal tangent curve (use parabola properties)

- If $S > L$ (you can see the end of the curve):



$$L_m = 2 \times SSD - \frac{200(\sqrt{H_1} + \sqrt{H_2})^2}{A}$$

SSD on Crest Curves

- AASHTO Guideline

- Sight distance ($S = \text{SSD}$)
- Driver's eyes ($H_1 = 3.5 \text{ ft}$)
- Height of an object ($H_2 = 2.0 \text{ ft}$)
- Equal tangent curve (use parabola properties)
- $A = |G_1 - G_2|$

For $\text{SSD} < L$

$$L_m = \frac{A \times \text{SSD}^2}{2158}$$

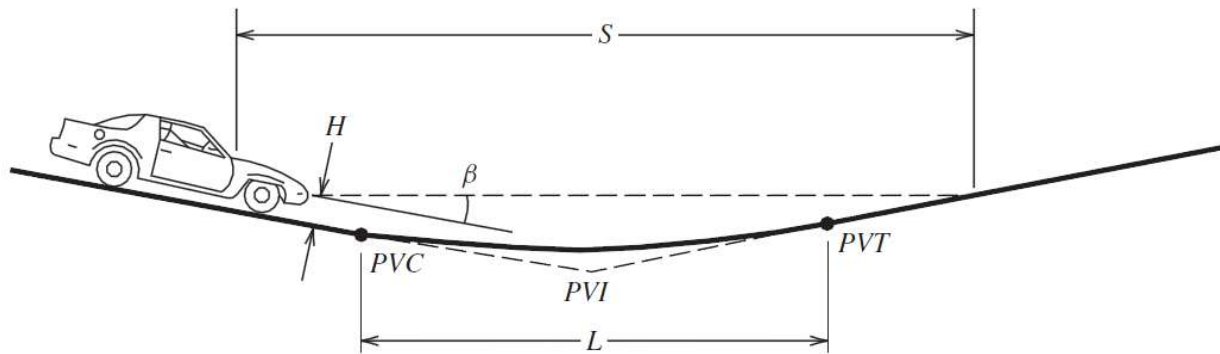
For $\text{SSD} > L$

$$L_m = 2 \times \text{SSD} - \frac{2158}{A}$$

SSD on Sag Curves

- Since SSD is unrestricted on sag curves during daylight hours, **nighttime conditions** govern design.
- Thus, the critical concern for sag curves is the **headlight sight distance** (i.e., the length of road illuminated by the vehicle's headlights).
- Which is a function of the **height of the headlight** above the roadway, H , and the **inclined upward angle of the headlight beam**, relative to the horizontal plane of the car, β

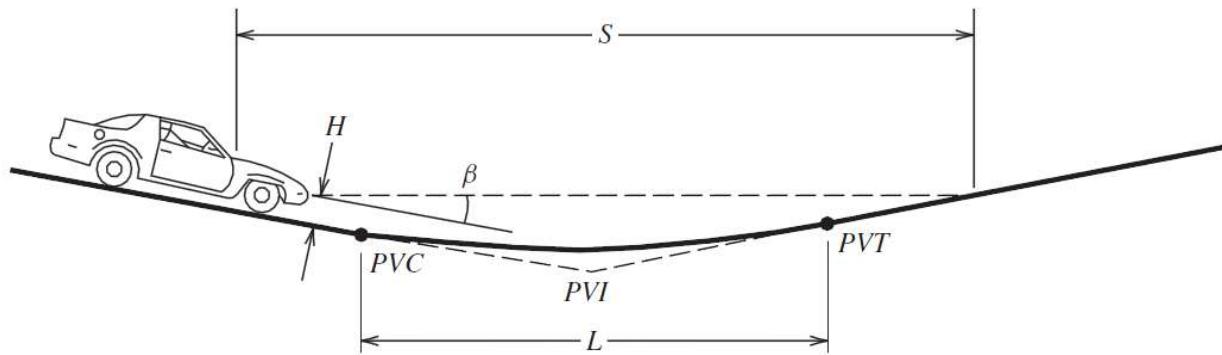
SSD on Sag Curves



- If $S < L$ (you can't see the end of the curve):

$$L_m = \frac{A \times SSD^2}{200(H + SSD \tan \beta)}$$

SSD on Sag Curves



- If $S > L$ (you can see the end of the curve):

$$L_m = 2 \times SSD - \frac{200(H + SSD \tan \beta)}{A}$$

SSD on Sag Curves

- AASHTO Guideline

- Assuming a headlight height ($H = 2.0$ ft) and an upward headlight angle ($\beta = 1^\circ$)
- $SSD = S$

$$SSD < L$$

$$L_m = \frac{A \times SSD^2}{400 + 3.5 \times SSD}$$

$$SSD > L$$

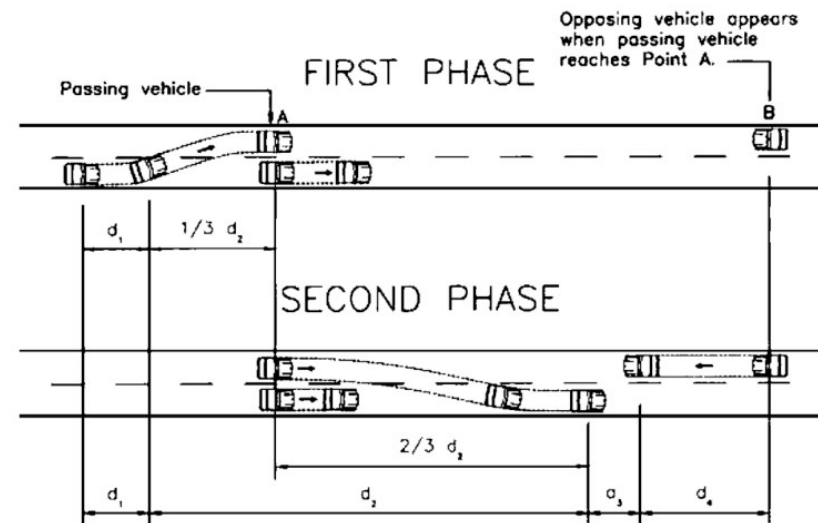
$$L_m = 2 \times SSD - \frac{400 + 3.5 \times SSD}{A}$$

Passing Sight Distance (PSD)

- Passing sight distance is important in 2-lane highway design
- Sight distance required for passing is generally much longer than required for stopping
- Assumptions
 - Constant speeds
 - Passing veh. speed > 10 mph from vehicle passing
 - $H_2 = 3.5$ ft.

Passing Sight Distance (PSD)

- d_1 : The distance the passing vehicle travels while **contemplating the passing maneuver**, and while accelerating to the point of encroachment on the left lane.
- d_2 : The length of roadway that is traversed by the passing vehicle **while it occupies the left lane**.
- d_3 : The **clearance distance** between the passing vehicle and the opposing vehicle when the passing vehicle returns to the right lane.
- d_4 : The **distance that the opposing vehicle travels** during the final 2/3 of the period when the passing vehicle is in the left lane.



For $PSD < L$

$$L_m = \frac{A \times PSD^2}{2800}$$

For $PSD > L$

$$L_m = 2 \times PSD - \frac{2800}{A}$$

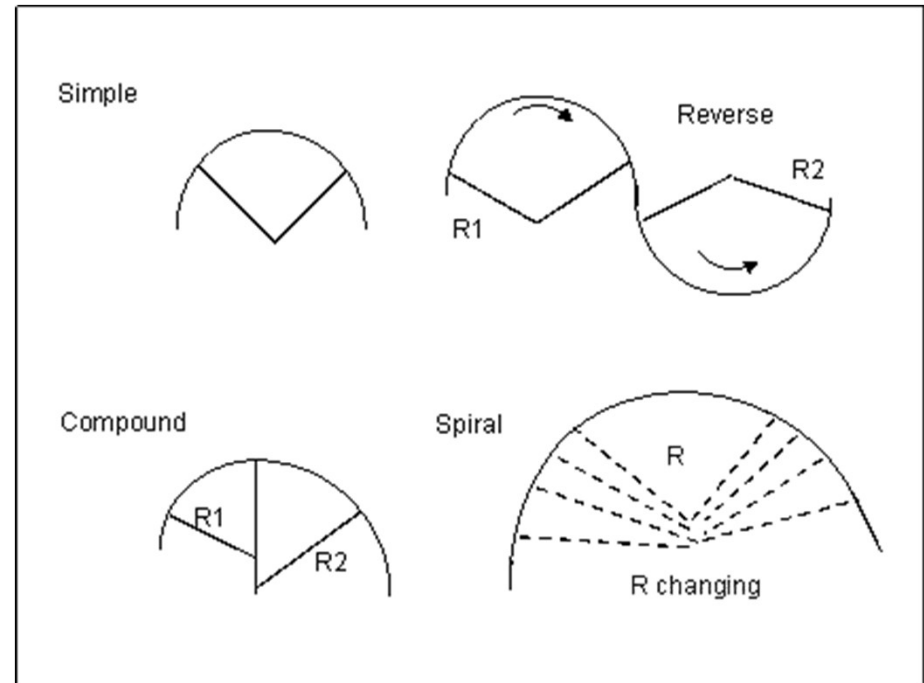


Horizontal Alignment

Curve Options

- Types of horizontal curves

- **Simple circular curve**
- Reverse curves
- Compound curves
- Spiral curves



Simple Circular Curve

R = radius, usually measured to the centerline of the road, in ft (m),

Δ = central angle of the curve in degrees,

PC = point of curve (the beginning point of the horizontal curve),

PI = point of tangent intersection,

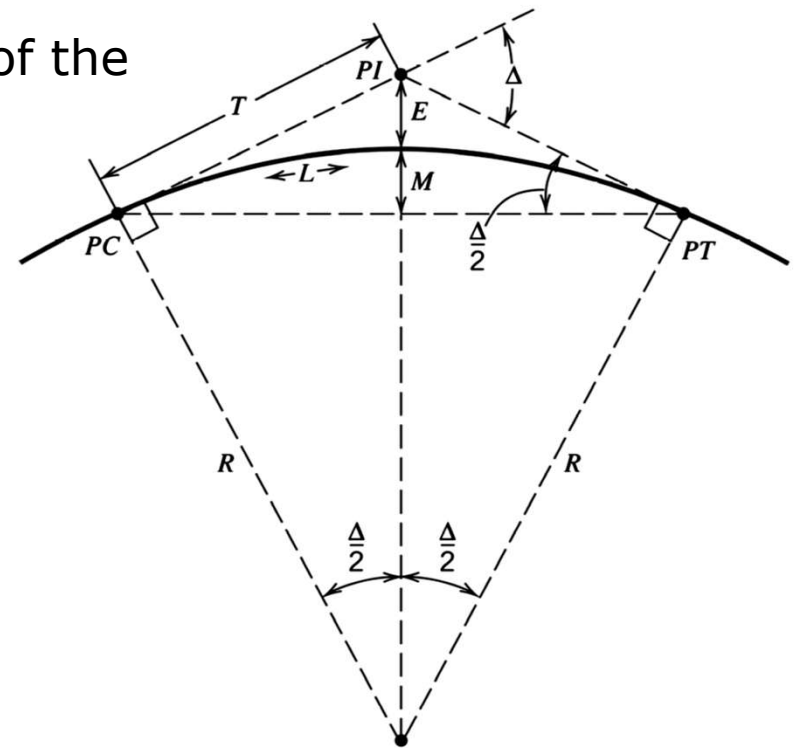
PT = point of tangent (the ending point of the horizontal curve),

T = tangent length in ft (m),

M = middle ordinate in ft (m),

E = external distance in ft (m), and

L = length of curve in ft (m).



Horizontal Curves

- **Vehicle cornering** capability is thus a key concern in horizontal curve design

R_v = radius defined to the vehicle's traveled path in ft (m),

α = angle of incline in degrees,

e = number of vertical ft (m) of rise per 100 ft (m) of horizontal distance,

W = weight of the vehicle in lb (N),

W_n = vehicle weight normal to the roadway surface in lb (N),

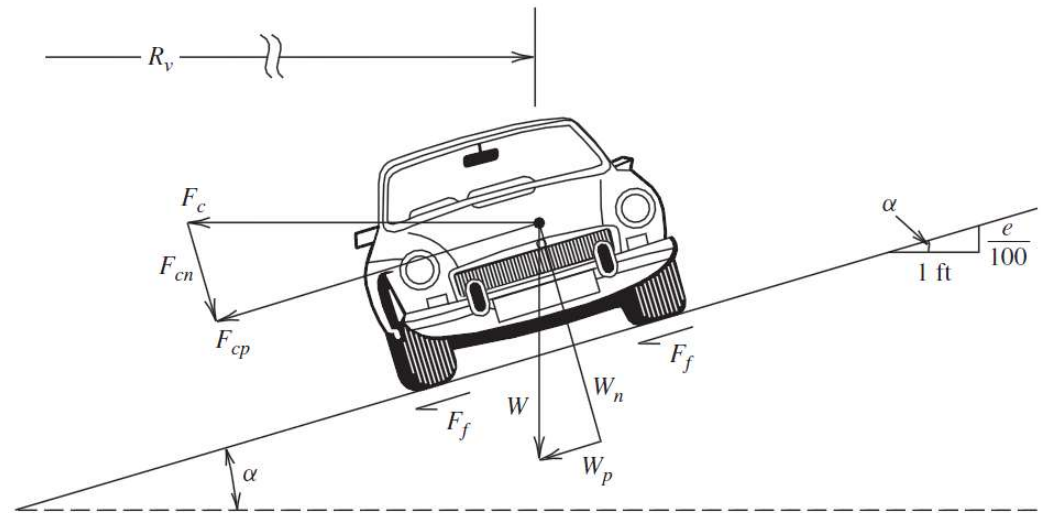
W_p = vehicle weight parallel to the roadway surface in lb (N),

F_f = side frictional force (centripetal, in lb (N)),

F_c = centripetal force (lateral acceleration x mass, in lb (N)),

F_{cp} = centripetal force acting parallel to the roadway surface in lb (N), and

F_{cn} = centripetal force acting normal to the roadway surface in lb (N).



Minimum Radius

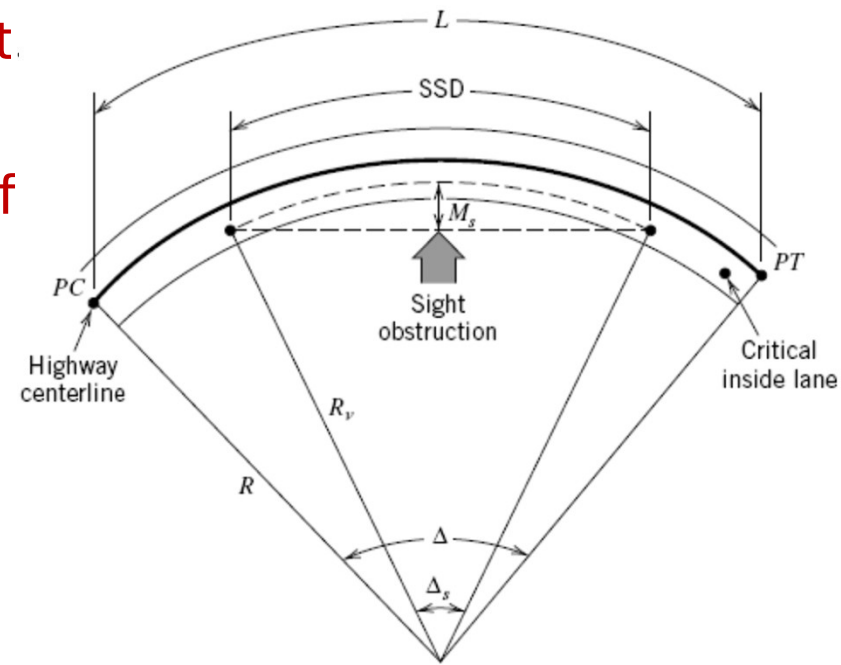
$$R_v = \frac{V^2}{g(f_s + \frac{e}{100})}$$

Table 3.5 Minimum Radius Using Limiting Values of e and f_s

Design speed (mi/h)	Maximum e (%)	Limiting values of f_s	Total $(e/100 + f_s)$	Calculated radius, R_c (ft)	Rounded radius, R_r (ft)	Design speed (mi/h)	Maximum e (%)	Limiting values of f_s	Total $(e/100 + f_s)$	Calculated radius, R_c (ft)	Rounded radius, R_r (ft)
10	4.0	0.38	0.42	15.9	16	10	10.0	0.38	0.48	13.9	14
15	4.0	0.32	0.36	41.7	42	15	10.0	0.32	0.42	35.7	36
20	4.0	0.27	0.32	86.0	86	20	10.0	0.27	0.37	72.1	72
25	4.0	0.23	0.27	154.3	154	25	10.0	0.23	0.33	126.3	126
30	4.0	0.20	0.24	250.0	250	30	10.0	0.20	0.30	200.0	200
35	4.0	0.18	0.22	371.2	371	35	10.0	0.18	0.28	291.7	292
40	4.0	0.16	0.20	533.3	533	40	10.0	0.16	0.26	410.3	410
45	4.0	0.15	0.19	710.5	711	45	10.0	0.15	0.25	540.0	540
50	4.0	0.14	0.18	925.9	926	50	10.0	0.14	0.24	694.4	694
55	4.0	0.13	0.17	1186.3	1190	55	10.0	0.13	0.23	876.8	877
60	4.0	0.12	0.16	1500.0	1500	60	10.0	0.12	0.22	1090.9	1090
10	6.0	0.38	0.44	15.2	15	65	10.0	0.11	0.21	1341.3	1340
15	6.0	0.32	0.38	39.5	39	70	10.0	0.10	0.20	1633.3	1630
20	6.0	0.27	0.33	80.8	81	75	10.0	0.09	0.19	1973.7	1970
25	6.0	0.23	0.29	143.7	144	80	10.0	0.08	0.18	2370.4	2370
30	6.0	0.20	0.26	230.8	231	10	12.0	0.38	0.50	13.3	13
35	6.0	0.18	0.24	340.3	340	15	12.0	0.32	0.44	34.1	34
40	6.0	0.16	0.22	484.8	485	20	12.0	0.27	0.39	68.4	68
45	6.0	0.15	0.21	642.9	643	25	12.0	0.23	0.35	119.0	119
50	6.0	0.14	0.20	833.3	833	30	12.0	0.20	0.32	187.5	188
55	6.0	0.13	0.19	1061.4	1060	35	12.0	0.18	0.30	272.2	272
60	6.0	0.12	0.18	1333.3	1330	40	12.0	0.16	0.28	381.0	381
65	6.0	0.11	0.17	1656.9	1660	45	12.0	0.15	0.27	500.0	500
70	6.0	0.10	0.16	2041.7	2040	50	12.0	0.14	0.26	641.0	641
75	6.0	0.09	0.15	2500.0	2500	55	12.0	0.13	0.25	806.7	807
80	6.0	0.08	0.14	3047.6	3050	60	12.0	0.12	0.24	1000.00	1000
10	8.0	0.38	0.46	14.5	14	65	12.0	0.11	0.23	1224.6	1220
15	8.0	0.32	0.40	37.5	38	70	12.0	0.10	0.22	1484.8	1480
20	8.0	0.27	0.35	76.2	76	75	12.0	0.09	0.21	1785.7	1790
25	8.0	0.23	0.31	134.4	134	80	12.0	0.08	0.20	2133.3	2130
30	8.0	0.20	0.28	214.3	214						
35	8.0	0.18	0.26	314.1	314						
40	8.0	0.16	0.24	444.4	444						
45	8.0	0.15	0.23	587.0	587						
50	8.0	0.14	0.22	757.6	758						
55	8.0	0.13	0.21	960.3	960						
60	8.0	0.12	0.20	1200.0	1200						
65	8.0	0.11	0.19	1482.5	1480						
70	8.0	0.10	0.18	1814.8	1810						
75	8.0	0.09	0.17	2205.9	2210						
80	8.0	0.08	0.16	2666.7	2670						

Stopping Sight Distance (SSD)

- Sight distance restrictions on horizontal curves occur **when obstructions are present**.
- When obstruction exists, **SSD is measured along the horizontal curve from the center of the traveled lane** (the assumed location of the driver's eyes).
- for a specified stopping distance, some distance, M_s (the **middle ordinate** of a curve that has an arc length equal to the stopping sight distance), **must be visually cleared** so that the line of sight is such that sufficient SSD is available.



Stopping Sight Distance (SSD)

$$\text{SSD} = \frac{\pi}{180} R_v \Delta_s \quad \rightarrow \quad \Delta_s = \frac{180 \times \text{SSD}}{\pi R_v}$$

Substituting into the general equation for the middle ordinate of simple horizontal curve (Eq. 3.38) gives

$$M_s = R_v \left(1 - \cos \frac{90 \times \text{SSD}}{\pi R_v} \right)$$

Solving the above equation for SSD gives

$$\text{SSD} = \frac{\pi R_v}{90} \left[\cos^{-1} \left(\frac{R_v - M_s}{R_v} \right) \right]$$

References

- Mannering, F., and S. Washburn (2020). Principles of Highway Engineering and Traffic Analysis, Seventh Edition, John Wiley & Sons
- American Association of State Highway and Transportation Officials (AASHTO). (2018). A Policy on Geometric Design of Highways and Streets (7th ed.). Washington, D.C.: AASHTO